AMENDMENTS TO THE SPECIFICATION

Please amend the paragraph beginning at page 5, line 21, as follows:

The inverter controller further includes: a motor voltage command generator which generates a motor voltage command value of the motor, based on a speed command value of the motor applied from the outside; a positive neutral (PN) ~~PN~~-voltage detector which detects a DC voltage value of the inverter; a PN voltage corrector which calculates a ratio of the DC voltage detection value of the inverter obtained by the PN voltage detector to a predetermined DC voltage reference value of the inverter to thereby generate a PN voltage correction factor; and a motor voltage command corrector which generates a motor voltage command correction value of the motor.

Please amend the paragraph beginning at page 9, line 25, as follows:

Fig. 11 is a block diagram showing a system constitution of a prior art ~~general~~-inverter controller for driving an induction motor;

Please amend the paragraph beginning at page 10, line 2, as follows:

Fig. 12 is a graph view showing an example of a prior art ~~general~~-V/F control pattern;

Please amend the paragraph beginning at page 10, line 4, as follows:

Fig. 13 is a diagrammatic view showing a relation between a harmonic component of an AC power supply current and an order to the AC power supply frequency in the prior art inverter controller shown in Fig. 11; and

Please amend the paragraph beginning at page 10, line 7, as follows:

Fig. 14 is a circuit diagram showing a prior art ~~conventional~~ DC power supply apparatus.

Please amend the paragraph beginning at page 14, line 16, as follows:

In addition, it is noted here that[[,]] the present invention is not limited to the inverter controller for driving the induction motor by the V/F control as described in the above embodiment, but can be applied to an inverter controller for driving an induction motor by a well-known vector control.

Please amend the paragraph beginning at page 15, line 16, as follows:

It is noted here that[[,]] the PN voltage correction factor k_{pn} does not always have both the upper limit value k_{pn1} and the lower limit value k_{pn2} as shown in Fig. 3, and it may have only one of them depending on an operation condition.

Please amend the paragraph beginning at page 16, line 15, as follows:

Here, Figs. 5 and 6 show results when the inverter controller for driving the induction motor according to the present invention is operated. Fig. 5 shows a result when neither an upper limit value nor a lower limit value is set in the PN voltage correction factor k_{pn}, and Fig. 6 is a result when both of the upper limit value and the lower limit value are set in the PN voltage correction factor k_{pn}. Comparing between reactor current waveforms (each showing a current after flowing through the diode bridge) in Fig. 5 and Fig. 6, its effect is apparent.

Please amend the paragraph beginning at page 19, line 11, as follows:

Fig. 7 shows a result when the inverter controller for driving the induction motor of the present embodiment is operated, which shows the operation result when the inverter operation frequency f_I becomes twice of ~~as~~ the AC power supply frequency f_S. In this operation, the resonant phenomenon is generated in synchronization with the frequency at which the inverter DC voltage fluctuates, and it is apparent that a negative DC component is superposed on the motor current in Fig. 7.

Please amend the paragraph beginning at page 20, line 2, as follows:

Thus, when, ~~when ,~~ in setting the inverter operation frequency f_I, it is necessary to prevent the inverter operation frequency f_I from being constantly fixed to a case shown by a formula (8).

Please amend the paragraph beginning at page 20, line 15, as follows:

It is noted here that[[,]] the frequency width Δf is not always required to be set, and it may not be set depending on the operation condition (such as light load state) (i.e., in this case, it may be set as $\Delta f = 0$).